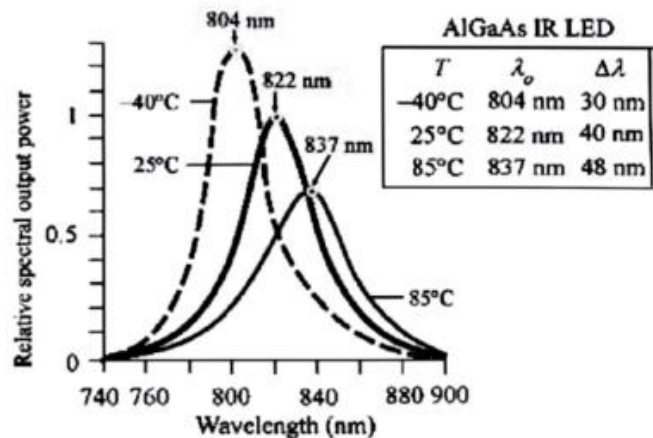


Sheet 3

1. Consider the three experimental points in the table shown in the Figure to the right. From problem 2, $\Delta\lambda$ varies linearly with T , that is:

$(\Delta\lambda/\lambda_0^2) = mKT/hc$. By a suitable plot find m and verify the relation of the linewidth $\Delta\lambda$ of the previous problem.



3) $\Delta E = \frac{hc}{\lambda^2}$ $\Delta\lambda = mKT$

$\left(\frac{\Delta\lambda}{\lambda^2}\right) = \frac{mKT}{hc}$

Slope = $\frac{(5.9 - 4.6) \times 10^{-4}}{298 - 233} = 200$

$200 = \frac{mK}{hc} = \frac{m \times 1.38 \times 10^{-23}}{6.625 \times 10^{-34} \times 3 \times 10^8}$

$m = 2.88$

2) We know that the spread of the **wavelengths** in the emission spectrum of an LED is related to the spread in the emitted **photon energies**. The emitted photon energy $h\nu = hc/\lambda$. Assume that the spread in the photon energies $\Delta(h\nu) \approx 3kT$ between the half intensity points. Show that the corresponding linewidth $\Delta\lambda$ between the half intensity points in the output spectrum is:

$$\Delta\lambda = \lambda_o^2 \frac{3KT}{hc} \quad \text{where "K" is the Boltzmann constant}$$

and λ_o is the peak emission wavelength.

What is the spectral linewidth of an optical communications LED operating at **1310 nm** and at **300 °k** ? (Note °k means degree Kelvin)

$$\begin{aligned} 2) \quad \Delta E &= \frac{hc}{\lambda^2} \Delta\lambda = 3kT \\ \Delta\lambda &= \lambda^2 \frac{3kT}{hc} = (1310 \text{ nm})^2 \times \frac{3 \times 300 \times 1.38 \times 10^{-23}}{6.625 \times 10^{-34} \times c} \\ \Delta\lambda &= 1.07 \times 10^{-7} \text{ m} \end{aligned}$$

3) Using the expression $E = hc/\lambda$, show why the Full Width at Half Maximum (FWHM) power spectral width of LEDs become wider at longer wavelengths.

Differentiating the expression for E , we have

$$\Delta E = \frac{hc}{\lambda^2} \Delta\lambda \quad \text{or} \quad \Delta\lambda = \frac{\lambda^2}{hc} \Delta E$$

For the same energy difference ΔE , the spectral width $\Delta\lambda$ is proportional to the wavelength squared. Thus, for example,

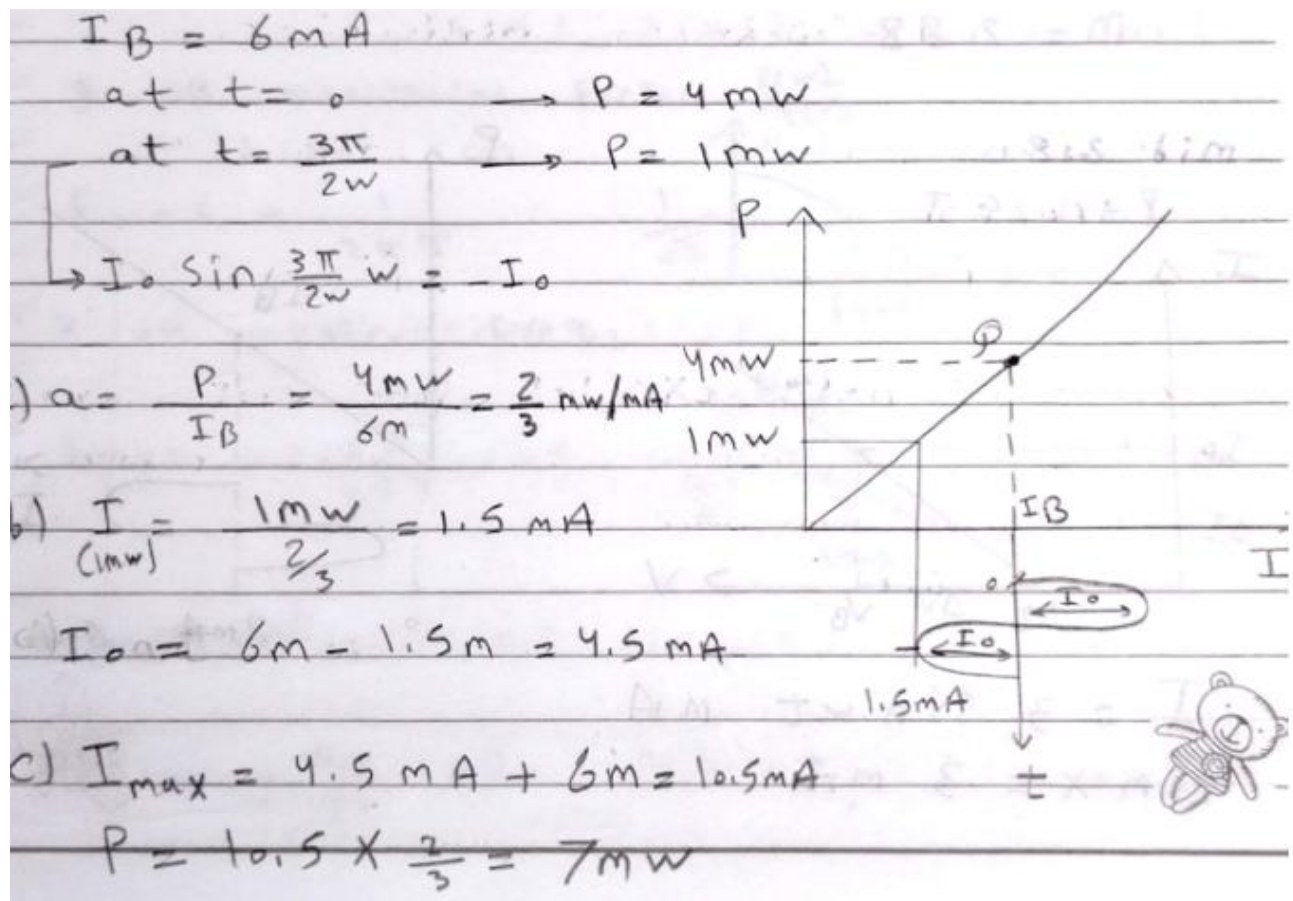
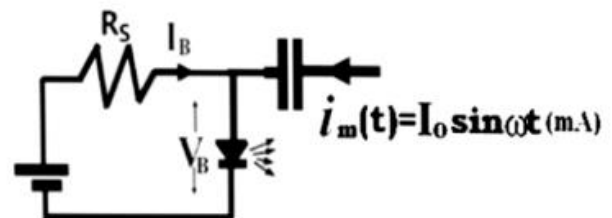
$$\frac{\Delta\lambda_{1550}}{\Delta\lambda_{1310}} = \left(\frac{1550}{1310} \right)^2 = 1.40$$

4. Assume that all the modulating current $i_m(t)$ flows through the LED. The bias current $I_B = 6 \text{ mA}$.

At the instant $t=0$, the instantaneous emitted output power is 4 mW . And at

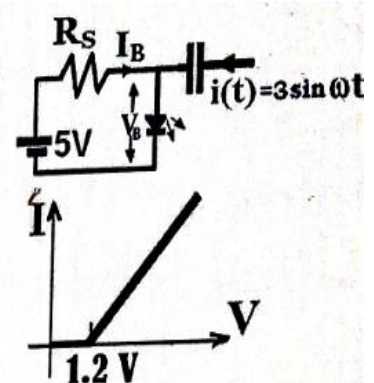
$t=3\pi/2\omega$, the instantaneous emitted output power is 1 mW . Calculate:

- The slope of the output Power-Current characteristic of the LED.
- The amplitude I_0 of the modulating current.
- The **maximum** instantaneous emitted power.



5. It is required to modulate the emitted output power from the LED shown in the figure by an AC current $i(t)=3\sin\omega t$ (mA). Accordingly, the LED must be biased by a DC current I_B such that the output light is not clipped (cutoff) during the negative part of $i(t)$. The LED has the approximate linear I-V characteristic shown in the figure, the slope of the line is 15 mA/V . (Assume that all the AC current $i(t)$ flows through the LED).

- What is the "minimum" value of I_B ? (15 marks)
- Calculate the DC voltage V_B across the LED. (10 marks)
- Calculate the value of the required resistor R_S . (5 marks)



- a) The negative part of the sin wave has an amplitude -3 mA. At this operating point the output "Power" decreases to 0 since the P-I characteristic is linear and starts from 0. Therefore, in order that the negative part be unclipped, the **total current** flowing through the LED at that instant should be 0. Thus, at $i(t) = -3 \text{ mA}$ the **total current**:

$$i = I_B + i(t) = I_B - 3 = 0, \text{ THUS: } \underline{I_B = 3 \text{ mA.}}$$

- b) From the (I-V) c/c of the LED, the voltage across the LED, should be above the cutoff (1.2V) by an amount ΔV corresponding to $I_B = 3 \text{ mA}$. And since the c/c is linear, then:

$$\text{Since the slope } 15 \text{ (mA/V)} = I_B / \Delta V$$

$$\therefore \Delta V = I_B / 15 \text{ (mA/V)} = 3 \text{ mA} / 15 \text{ (mA/V)} = 3/15 \text{ V} = \underline{0.2 \text{ V.}}$$

$$\therefore V_B = 1.2 + \Delta V = 1.2 + 0.2 = \underline{1.4 \text{ V}}$$

- c) Since the voltage across R_S is:

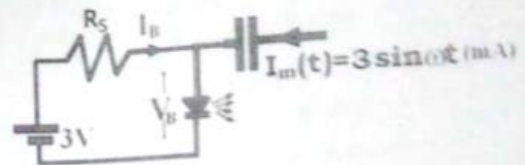
$$(V_S - V_B) = 5 - 1.4 = 3.6 \text{ V}$$

$$\therefore R_S = (V_S - V_B) / I_B = 3.6 \text{ V} / 3 \text{ mA} = \underline{1200 \Omega}$$

6. The P-I characteristic of a certain LED is described by: $P = aI$ where $a = 1.25 \text{ mW/mA}$. Its I-V characteristic is

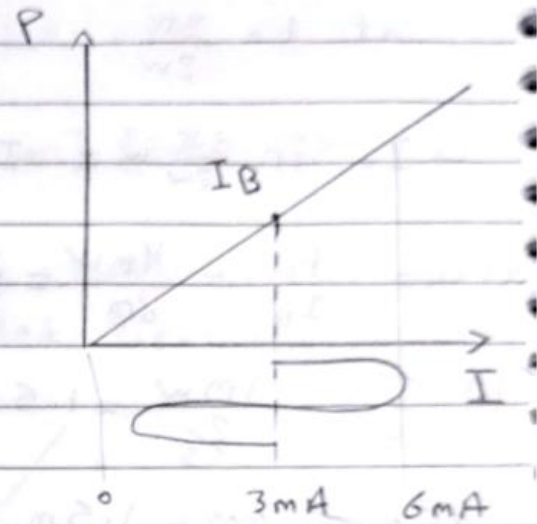
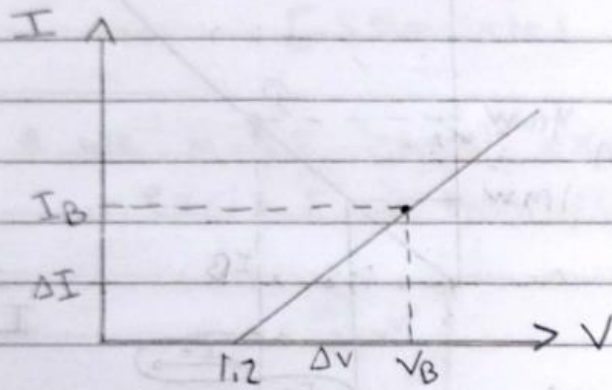
$$\text{described by: } \begin{cases} I = 0 & \text{for } 0 \leq V \leq 1.2 \text{ V} \\ I = bV & \text{for } V \geq 1.2 \text{ V} \end{cases}$$

Assume that $b = 16 \text{ mA/V}$, and that all the AC modulating current passes through the LED. Calculate the "lowest" possible value of the LED quiescent point (I_B and V_B) and the resistor R_S .



mid 2.18

$$P = 1.25 I$$



$$I = 3 \sin \omega t \text{ mA}$$

$$I_{\max} = 3 \text{ mA}$$



P at max P point, 3 mA

$$P = 1.25 I = 1.25 \times 3 \text{ m} = 1.875 \text{ mW}$$

$$\Delta I = 16 \text{ m} \Delta V$$

$$3 \text{ m} = 16 \text{ m} \Delta V, \Delta V = 0.19 \text{ V}$$

$$V_B = \Delta V + 1.2 = 1.39 \text{ V}$$

$$R_S = \frac{3 - 1.39}{3 \text{ m}} = 537 \Omega$$